WAVEMILL PROOF-OF-CONCEPT DATA ANALYSIS NEAR MERSEY BAR LIGHT

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2 WAVE ARTEFACT VELOCITY MODEL

3 DATA ANALYSIS

- Inter-run Analysis
- Intra-run Analysis





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4 Conclusions & Perpectives



AREA & CONFIGURATION





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- ADCP at 2-4m
- HF radar (current & wind direction)
- Wave Spectrum up to 5m wavelength
- MetOffice Wind @1.5km;1h





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Chapron et al., 2005

$$T(\varphi,\theta) = \frac{G(\varphi,\theta)}{\tan\theta} \int_{k} k\omega S(\vec{k}) d\vec{k}$$

MODEL INPUT:

- G: Gain factor derieved from Geophysical Model Function of NRCS interpolated between CMOD5 and NSCAT for X-band
- S: Directional wave spectrum (buoy + KHCC)





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WAVE ARTEFACT VELOCITY — GAIN FACTOR



- |G| decrease with incidence angle
- |G| decrease with wind speed
- |G| downwind > upwind

WAVE ARTEFACT VELOCITY — WAVE SPECTRUM

$$T(\varphi, \theta) = \frac{G(\varphi, \theta)}{\tan \theta} \int_{k} k\omega S(\vec{k}) d\vec{k}$$
$$S(\vec{k}) = S(k, \varphi) - S(k, \varphi - \pi)$$



Sensitivity maximum to wave around 10m of wavelength

perfect symmetry of 180° of wave component

WAVE ARTEFACT VELOCITY — MODEL USING BUOY



- Amplitude decrease with incidence angle
- Amplitude decrease slightly when wind speed increase
- Azimuthal signal dominated by up/downwind variation
- Downwind > upwind magnitude opposite to observations
 - derived from Gain factor

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METHODS



HYPOTHESIS

- Homogeneous geophysic conditions
- No XT baseline component or topography effect

- Median along track of the run's portion for:
 - SLC amplitude
 - Interferogram



SLC AMPLITUDE



- SLC amplitude azimuthal variation in accordance with a southerly wind (for each incidence angle)
- Amplitude discrepancies between Fore and Aft antennae
- Post calibration of antennae using the omnidirectional component ('a' factor) does not improve agreement between antennae (not shown).

INTERFEROGRAMS



- Azimuth and incidence angle vary together, difficult interpretation
- For similar range (circle or triangle) and azimuth => good agreement between antennae



INTERFEROGRAMS TO SURFACE COMPONENT VELOCITY



- Figure combine surface current velocity, wave artefact velocity, azimuth and incidence angle variation
- => remove surface current velocity from ADCP

WAVE ARTEFACT VELOCITY - FROM DATA



- Amplitude decrease with incidence angle
- Amplitude maxima in up/downwind direction (agreement with model)
- Upwind amplitude > downwind (opposite with model but agreement with ASAR data [Mouche et al., 2012])

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DATA ANALYSIS Inter-run Analysis

Intra-run Analysis

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INTRA-RUN VARIABILITY — SLC AMPLITUDE

Amplitude corrected for incidence angle dependency — averaging to 100m



No obvious consistent features



INTRA-RUN VARIABILITY

STARLAB-DERIVED VELOCITY



- Trend for the aft antenna derived-velocity, probably due to wind-wave fetch effect (not seen on other run)
- Velocity anomaly of both antennae highly correlated with aircraft rolling angle (0.03 m/s per ° of roll angle)
 - Surprisingly as SAR is installed on a gimbal (corrects aircraft roll) 20/2

Run 6 - NW -> SE - high aircraft drift variation



 High correlation of near minus far range difference between fore and aft antennae

seems to be linked to aircraft drift variation (gimbal corrects yaw)

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CONCLUSIONS & PERSPECTIVES

CONCLUSIONS

- Wind-wave artefact (X-band) in very good agreement with ENVISAT empirical data (C-band)
 - despite very specific condition during Irish Sea experiment (fetch, crossing sea)
- Variation with incidence angle and phase with wave in agreement with a simple theoretical model [Chapron et al., 2005]

FUTURE WORK

- More airborne flights with various geophysical conditions (open ocean)
- Inversion of both wind and current
 - need for calibrated sigma0
 - need for VV + HH polarisation
 - difference between X and Ku-band probably small. Need to be confirmed